

**B-4**

**C** **W** **M** **M** **M** **M**



## Memorandum

Foth Infrastructure & Environment, LLC  
2121 Innovation Court, Suite 300  
P.O. Box 5126 • De Pere, WI 54115-5126  
(920) 497-2500 • Fax: (920) 497-8516  
[www.foth.com](http://www.foth.com)

August 24, 2017

TO: Andrew Boushy, Aquila Resources Inc.

CC: Steve Donohue, Foth Infrastructure & Environment, LLC  
Master File

FR: Kris Baran, Foth Infrastructure & Environment, LLC  
John Starke, Foth Infrastructure & Environment, LLC  
Raymond Wong, Foth Canada Corporation

RE: Back Forty Project Design of Cut-off Wall/River Road Realignment/East Access  
Power Corridor - Revised

### Introduction

Aquila Resources Inc. (Aquila) is preparing a Mining Permit Application (MPA) for the Back Forty Project, which is located in western Menominee County, about 15 miles northwest of Stephenson, Michigan. The project consists of mining a volcanogenic massive sulfide deposit of zinc and copper as an open pit. The planned open pit is bounded to the west by the Menominee River. A cut-off wall is proposed to restrict seepage from the Menominee River to the open pit and improve the stability of the pit slope. Figure 1 shows the general location of the open pit, proposed cut-off wall alignment, and proposed River Road termination.

This memorandum presents the Permit Level design for the Menominee River cut-off wall based on the finalized open pit configuration by Aquila. The work is based on preliminary geotechnical investigation and cut-off wall alternative evaluation completed by Golder Associates Inc. in 2011 (Golder, 2011). From the preliminary concept description prepared by Golder, as well as the updated pit shell included with the Preliminary Economic Analysis (PEA) ( Tetra Tech, 2014), Foth has prepared the cut-off wall design to support the MPA including:

- ♦ Layout the cut-off wall alignment based on the finalized open pit configuration (Pit 32).
- ♦ Finalize the construction method and cut-off wall mix design.
- ♦ Update seepage estimates based on the realigned length and depth of the cut-off wall.

Design of the cut-off wall containment structure.

Determine optimum overburden slope configuration.

## **Previous Geotechnical Investigation and Study**

In 2011 Golder was retained by Aquila to provide technical support on a cut-off wall design to minimize seepage from the adjacent Menominee River into the planned open pit. A geotechnical investigation for the cut-off wall design was carried out in 2011. The scope of work covered by Golder's evaluation includes the following:

Evaluating preliminary seepage analyses and determining the need for a cut-off wall structure.

Comparing concept alternative cut-off wall construction methods with respect to constructability, performance (efficiency), environmental impact/footprint, order of magnitude construction cost, and potential requirement for bedrock grouting based upon previous mine description.

Recommend technically feasibility cut-off descriptions for the project.

## **Cut-off Wall Design**

### Design Basis

The cut-off wall is designed and constructed as a low permeability barrier through the overburden soils to impede seepage from the Menominee River into the proposed open pit and at the same time to reduce the hydraulic gradient in the overburden soil to improve slope stability. The selection of the type of cut-off wall construction technique shall be based on the ability of such method to excavate the on-site soils and rock in an efficient manner and provide the best performance as a low permeability barrier.

The pertinent design criteria of the Back Forty project cut-off wall are presented in Table 1.

**Table 1**

### **Cut-off Wall Design Criteria**

Description	Design Value
Maximum hydraulic conductivity	$\text{m/s}$
Minimum compression strength	tons/ $\text{feet}^2$
Minimum embedment depth in weathered rock	$\text{ft}$
Design maximum flood level of the Menominee River for a 100-year, 24-hour storm (Foth, 2015)	212 m
Minimum set-back distance (100 feet) to the	maximum
	flood level, i.e., 212 m

m/s = meter per second

Prepared by: RXW

feet $^2$  = square feet

Checked by: MJV2

m = meter

### Cut-off Wall Types

Four (4) cut-off wall construction alternatives were considered for the Back Forty Project including:

- Conventional Excavation (long-reach excavator).
- Clamshell Excavation.
- Cutter Soil Mixing (CSM).
- Trench Cutter (TC).

Of these, it is concluded that the CSM and the TC methods are best suited for constructing the cut-off wall in the soil and bedrock conditions present at the Project site. The Conventional Excavation and Clamshell Excavation methods were rejected due to limitations as outlined below:

- Difficult to control verticality.
- Not suitable for dense/stiff soils, cobbles and boulders.
- Cannot excavate bedrock.
- Cleaning if bottom of wall difficult.
- Difficult to ensure backfill quality to meet QA/QC.

The CSM and TC construction methods are capable of cutting through the bedrock to provide the necessary key-in in a single step. The CSM and TC construction methods are very similar, both employing cutting wheels rotating about a horizontal axis. The main difference between TC and the CSM is the manner the cut-off is formed. With the TC method, there is no injection of slurry at the point of cutting. Instead, cutting takes place under a head of bentonite slurry with the cut soils being removed from the trench by pumping to the surface in a suspension of a bentonite slurry. The TC method is usually used where very deep penetration (up to 120 m) in dense or bedrock formation is required. The CSM mixes the in-situ soils with cement-bentonite (SCB) slurry that is injected directly into the soil at the point of cutting. However, the capability of the CSM to penetrate the weathered zone is highly dependent on the strength of the bedrock encountered during construction of the cut-off wall. In the event that the CSM cannot penetrate the weathered zone to construct the cut-off wall key-in, the bottom 2 m (6 feet) of the cut-off wall shall be pressure grouted.

The CSM and TC method also provides a better assurance of quality and performance and has many advantages over the conventional and clamshell method. Based on the soil conditions and depth of the overburden, the CSM method is best suitable at the Project site.

### Cut-off Wall Alignment and Location

The general plan arrangement and profiles of the cut-off wall are shown on Figure 2. Typical cross sections through the cut-off wall alignment are provided on Figure 3. The depth of the cut-off wall varies from about 12 m to 20 m below the existing ground surface. The cut-off wall will have a setback distance of 30.5 m (100 feet) from the 100-year, 24-hour flood level, i.e., 212 m. Other environmental features such as cultural resources that could be affected by the pit cut-off wall are also shown on Figure 2.

### Cut-off Wall Construction

Figure 4 shows typical construction details of the cut-off wall. The CSM equipment shall be provided with a level platform during excavation of the cut-off trench to ensure verticality. A reinforced concrete guide wall is usually construed first to ensure that the CSM will properly be aligned. The guide wall also provides support of the near surface soil and footings for personnel and equipment. The cut-off wall is constructed in alternative panels. Two primary panels are constructed first. When the soil, cement, and bentonite (SCB) have set, the secondary panel is installed by overlapping into the primary panels, thus providing a continuous wall structure. The CSM is capable of excavating rock. However, in the event that it cannot penetrate unexpected hard formation, the cut-off wall will terminate at the rock surface and that a grout curtain shall be installed in the rock from the bottom of the cut-off wall. The depth of the grout curtain is the same as the embedment depth of the cut-off wall into weathered rock.

### Cut-off Wall Mix Design

The cut-off wall will be constructed of soil, cement, and bentonite mix (SCB). Typical bentonite mix content is 6% to 7% of cement by weight and the water/cement ratio shall be between 2 and 3. The final design mix should be determined by suitability tests prior to construction to ascertain that the SCB mix will meet the minimum hydraulic conductivity and a shear strength requirement to meet the final design criteria.

### Groundwater Seepage Estimate

Preliminary seepage analyses, based on the proposed cut-off wall profile, approximately 400 m in length indicated the seepage through the cut-off wall ranges from 123 to 4,756 cubic meters per day (32,500 to 125,500 gallons per day [gpd]) during Life of Mine. Further detailed seepage analyses will be carried out in the ongoing project hydrogeological evaluation. Groundwater infiltration and surface water runoff will be collected in sumps located at the lowest operating pit level. Pumps installed in the sumps will pump water to the clarifier ponds located near the Contact Water Basin (CWB). Pump design capacity will be determined with the Project final design upon completion of detailed water seepage analysis.

### Overburden Slope Stability

The overburden at the proposed cut-off wall location consists of loose to very dense silty sand to sand and gravel. Pockets of cobles were also encountered at some of the borehole locations. The thickness of the overburden varied from 11 to 21 m. The measured ‘N’ values from the Standard Penetration Test (SPT) of the overburden varied from 3 to more than 100 blows per 0.3 m of penetration. Copies of the boring logs from Golder (Golder, 2011) are provided in Attachment 1.

Based on SPT ‘N’ values and experience of the types of overburden, the geotechnical parameters adopted for slope stability analysis are presented in Table 2.

**Table 2**  
**Geotechnical Parameters Used for Slope Stability Analysis**

Description of Stratum	Unit Weight (kN/m <sup>3</sup> )	Cohesion, c' (kPa)	Internal Friction, φ(degrees)
Overburden	20	0	30
Cut-off Wall	20	500	30
Rock Fill Berm	20	0	36

Prepared by: RXW  
 Checked by: MJV2

The proposed overburden slope above the bedrock surface is 2H:1V and the toe is located a minimum of 15 m from the crest of the open pit slope. This provides a safe distance from the edge of the pit due to potential development of tension crack on the pit slope. To take into consideration of construction and normal road traffic, a surcharge load of 40 kPa is applied to the top of the slope.

Slope stability analyses were carried out using SLOPE/W software developed by Geo-Slope (Geo-Slope, 2012). The analyses were carried out for the following scenarios:

Static short-term condition when the slope is being formed and prior to the construction of the cut-off wall and the phreatic surface is based on the normal water level of the Menominee River.

Phreatic surface developed from a steady state flow condition during the 100-year, 24-hour storm with the cut-off wall in place. The raised water level of the Menominee River during the 100-year, 24-hour storm is assumed to be 212 m. For added stability and prevention of sloughing of the overburden slope face, a 3 m wide rock fill toe berm is provided downstream of the overburden slope. The rock fill berm toe is placed directly on bedrock and extended to elevation 210 m. Details of the overburden slope are shown on cross sections presented on Figure 3.

The minimum required factors of safety (FS) for slope stability are as follow:

FS during construction of the cut-off wall is 1.25; and  
 Long-term FS during a 100-year, 24-hour storm event is 1.5.

The results of slope stability analysis are provided in Attachment 2. All FS satisfy the minimum required and are summarized as below in Table 3.

**Table 3**  
**Summary of Overburden Slope Stability Analysis**

Description	FS
Static Short-Term Condition during Construction	27
Static Steady State with a 100-year, 24-hour storm event	1.62
	Prepared by: RXW Checked by: MJV2

### **Final Design and Construction Considerations**

The cut-off alignment will be placed to meet local zoning requirements as well as the project site development needs. The construction of the cut-off wall by the CSM method is often carried out by a specialty contractor. A common design build approach can accept this method based on performance criteria set out by the geotechnical engineer. Additional boreholes will be required at the southern-most portion of the cut-off wall to provide the level of confidence required for final design and tender prior to construction.

### **Proposed River Road Termination**

River Road is proposed to be terminated on the north and south sides of the mine pit during operations as shown on Figure 1. This proposal is currently being evaluated by the Menominee County Road Commission. If the proposed route is approved, all permitting will be handled by the Menominee County Road Commission as a separate project.

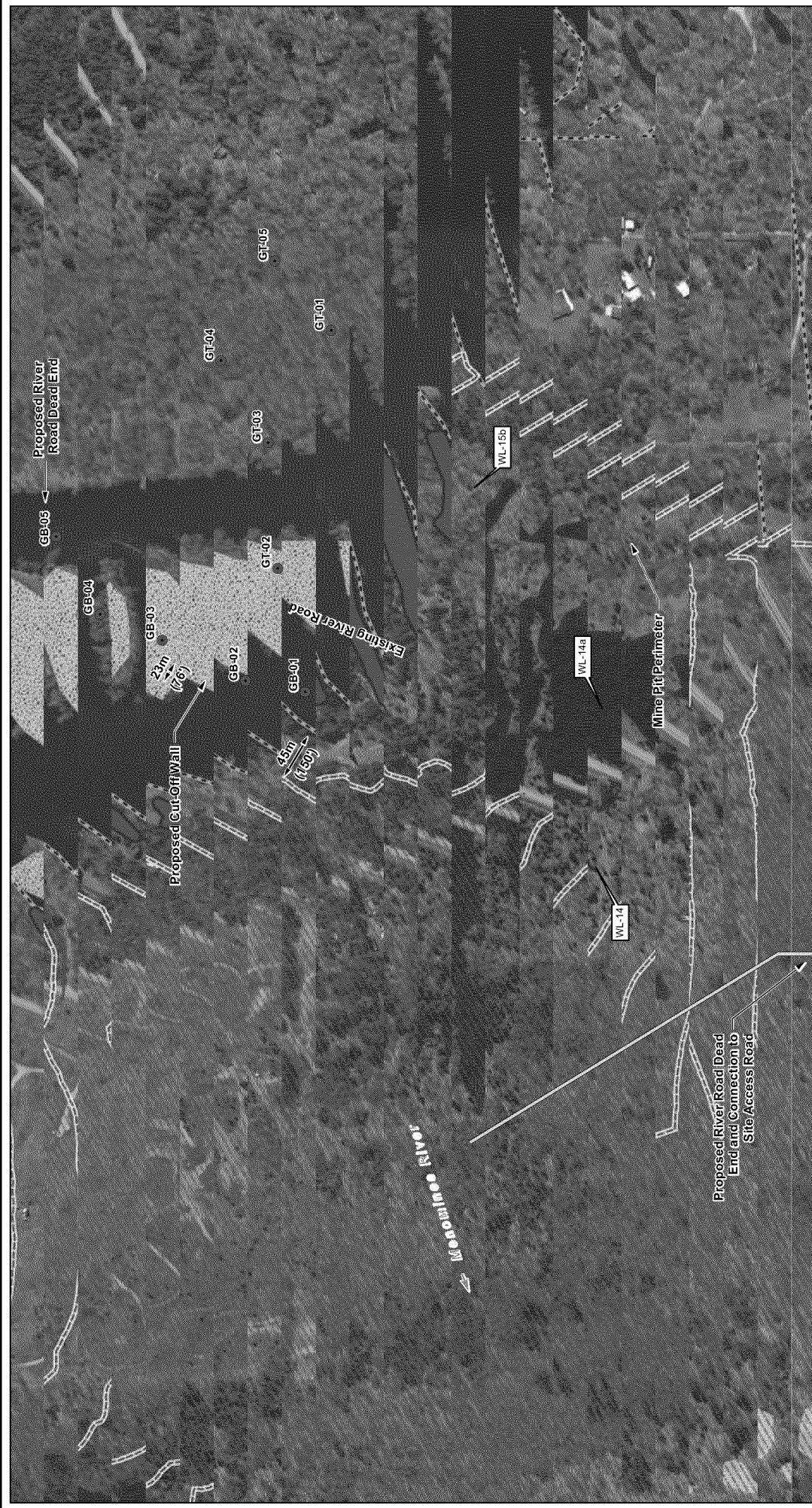
### **References**

- Foth Infrastructure & Environment, LLC, 2015. *Environmental Impact Assessment, Back Forty Project*. October 2015.
- Geo-Slope International, 2012. Calgary, Alberta, Canada.
- Golder Associates Inc., 2011. *Cut-off Wall Geotechnical Investigation Factual Report, Back Forty Project*. October 2011.
- Tetra Tech, 2014. *Preliminary Economic Assessment of the Back Forty Project, Michigan, USA*. July 23, 2014.

#### Attachments:

- Figure 1 – Cut-off Wall Alignment along Menominee River
- Figure 2 – Cross Section Locations and Longitudinal Cross Section
- Figure 3 – Transverse Cross Sections
- Figure 4 – Typical Cut-off Wall Section Detail
- Attachment 1 – Boring Logs
- Attachment 2 – Slope Stability Analysis Results

## **Figures**



Footh Infrastructure & Environment, LLC				BACK FORTY PROJECT			
REVISED	DATE	BY	DESCRIPTION				
				<b>FIGURE 1</b> CUTOFF WALL ALIGNMENT ALONG MENOMINEE RIVER STEPHENSON, MICHIGAN			
PREFERRED BY:	MJV2		DATE: SEP '17	Scale: 0	150	300	Date: SEPTEMBER 2017
APPROVED BY:	MAN		DATE: SEP '17	Drafted By:	DAT		Project No.: 17AO21
APPROVED BY:	KKB		DATE: SEP '17				

**NOTES**

1. Topographic and planimetric data provided by Aero-Metric, Inc., Sheboygan, WI.  
Date of Acquisition: LIDAR-October 21, 2007 and 2008.
2. Imagery May 14, 2008.
3. Horizontal coordinate datum based on NAD 1983.
4. Vertical coordinates in meters.
5. Wetlands categorized from July 2007 field surveys using the National Elevation Dataset.
6. Lycopodium sp. was collected in August 2011.
7. Cultural resources findings supplied by CCRG in 2011.

NOTES

BACK FORTY PROJECT

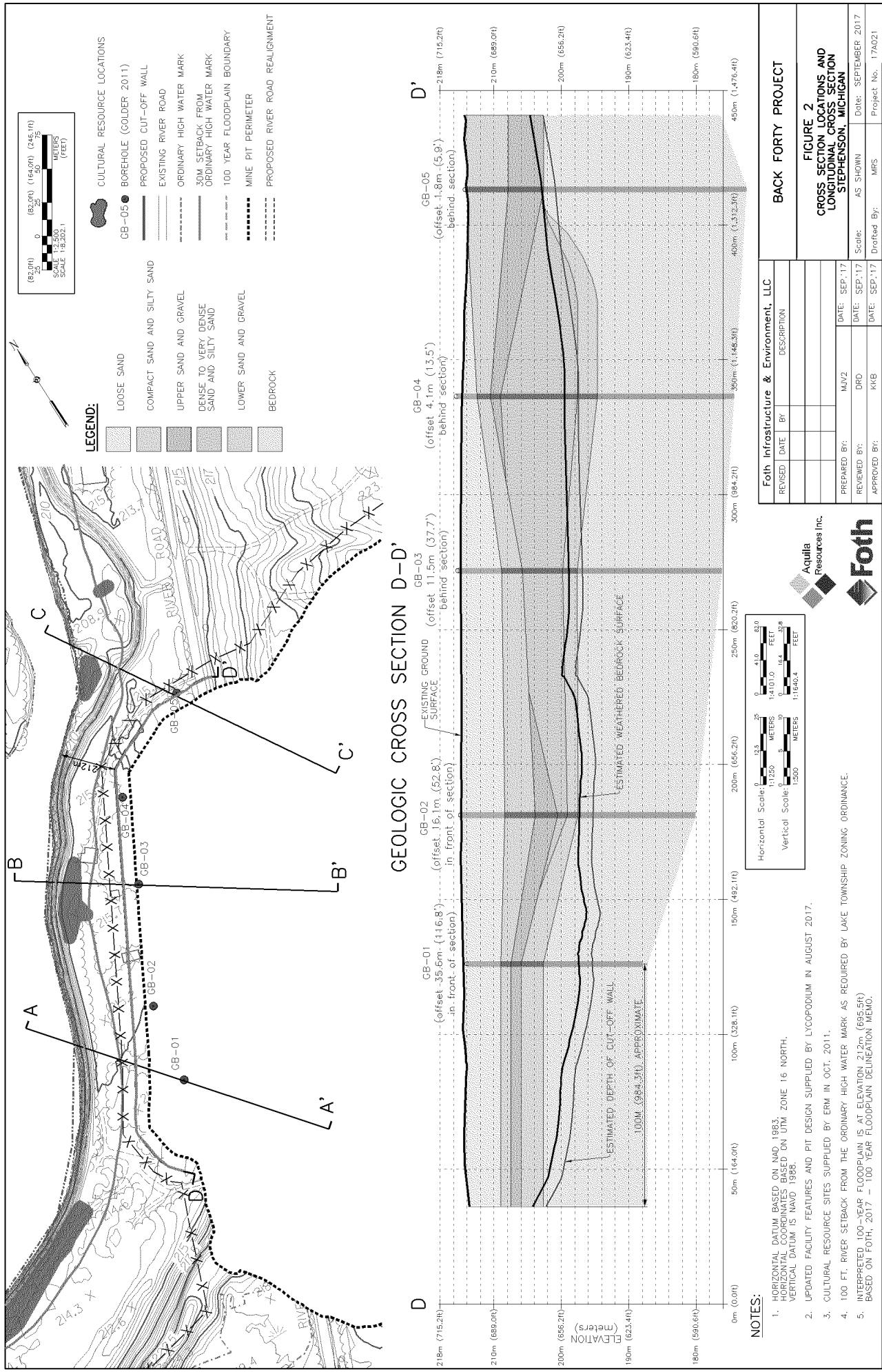
**FIGURE 1**

CUTOFF WALL ALIGNMENT  
ALONG MENOMINEE RIVER  
STEPHENSON, MICHIGAN

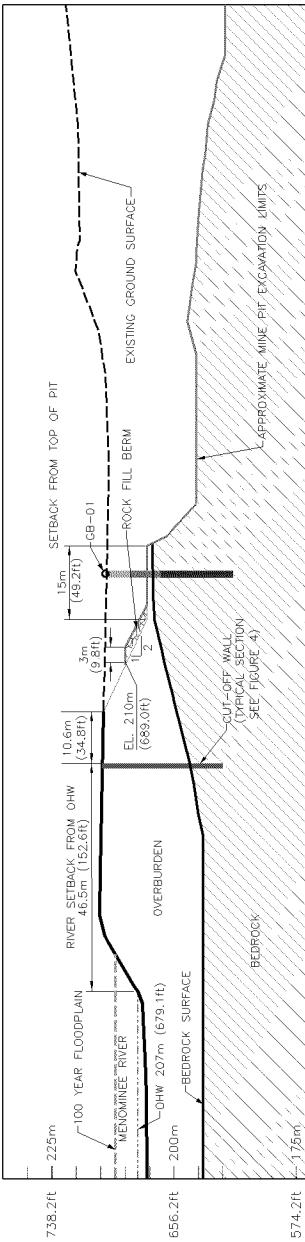
Project No.: 1

1160

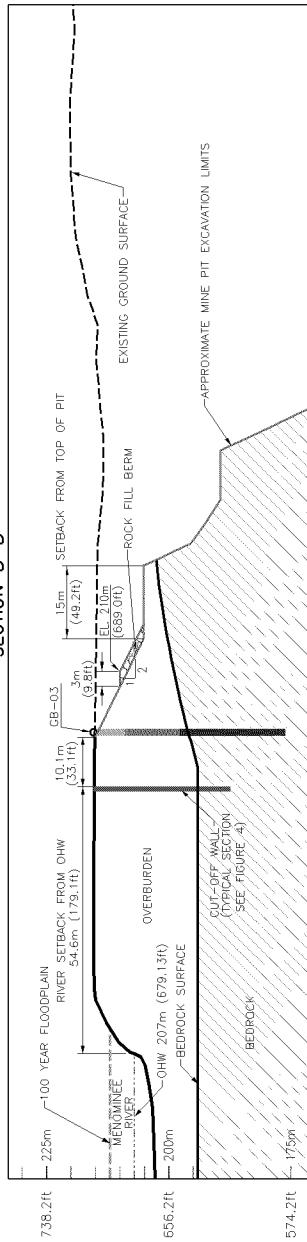
Path: X:\GB\NE\2014\14A021-001\G1Sum\dwPA\Aug 2017\Appendix B\Figure 1 Cut-Off Wall Alignment.mxd Date: 9/26/2017



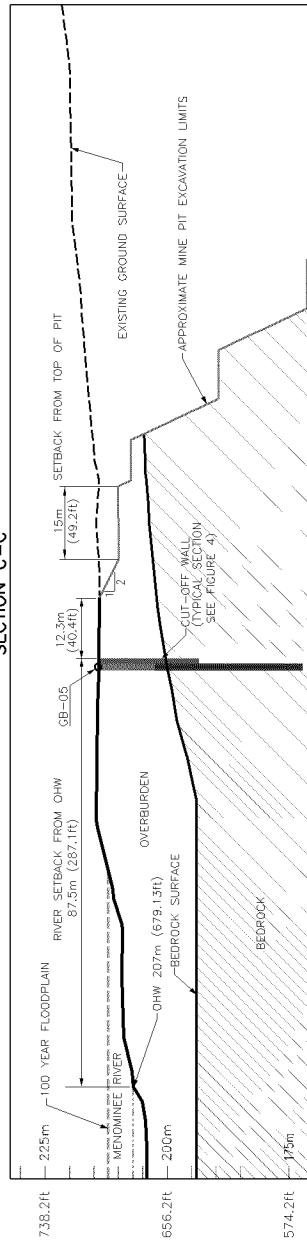
### SECTION A-A'



### SECTION B-B'



### SECTION C-C'



#### NOTES:

1. HORIZONTAL DATUM BASED ON NAD 1983. HORIZONTAL COORDINATES BASED ON UTM ZONE 16 NORTH.  
VERTICAL DATUM IS NAVD 1988.
  2. UPDATED FACILITY FEATURES AND PIT DESIGN SUPPLIED BY LYCOPIDIUM IN AUGUST 2017.
  3. CULTURAL RESOURCE SITES SUPPLIED BY FIRM IN OCT. 2011.
  4. 100ft. RIVER SETBACK FROM THE ORDINARY HIGH WATER LEVEL AS REQUIRED BY LAKE TOWNSHIP ZONING ORDINANCE.
  5. ORDINARY HIGH WATER MARK REPRESENTS THE SEASONALLY HIGH WATER MARK AND CAN GENERALLY BE TAKEN AS THE TYPICAL SHORELINE.
  6. CROSS SECTION LOCATIONS SHOWN ON FIGURE 2.
  7. INTERPRETED 100-YEAR FLOODPLAIN IS AT ELEVATION 212m (695.5ft)  
BASED ON FOTH, 2017 – 100 YEAR FLOODPLAIN DELINEATION MMCO.
- X:\G\PROJECT\14402-30\CAD\WPA\Aug 2017\Appendix CAD\Figure 3-Cut-off Wall Section.dwg  
9/27/2017

Foth Infrastructure & Environment, LLC		Back Forty Project	
REvised Date	Description	REV'D	

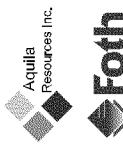
**FIGURE 3**  
**TRANSVERSE CROSS SECTIONS**  
**STEPHENSON, MICHIGAN**

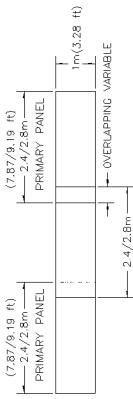
Date: SEPTEMBER 2017

Project No.: 17A021

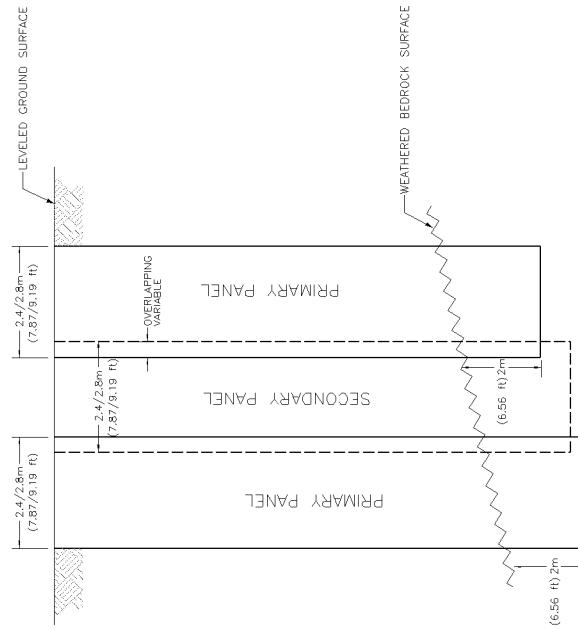
MRS

Drafted By:

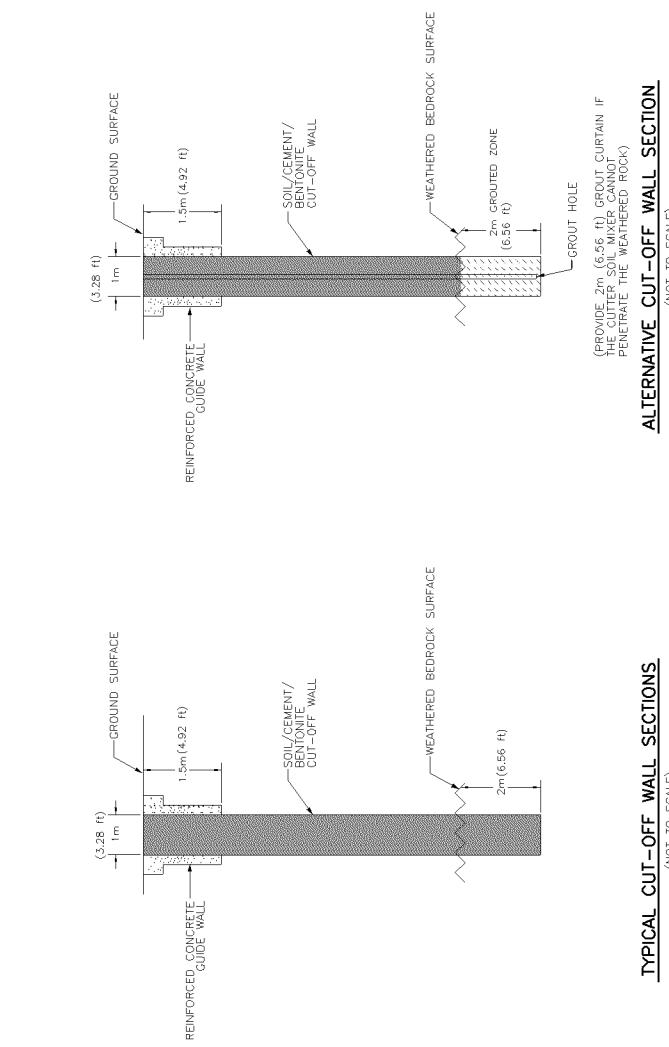




CUT-OFF WALL CONSTRUCTION SEQUENCE – PLAN VIEW  
(NOT TO SCALE)



CUT-OFF WALL CONSTRUCTION SEQUENCE – SECTION VIEW  
(NOT TO SCALE)



TYPICAL CUT-OFF WALL SECTIONS  
(NOT TO SCALE)

ALTERNATIVE CUT-OFF WALL SECTION  
(NOT TO SCALE)

NOTES:

- CONSTRUCTION METHOD ASSUMED TO BE CUTTER SOIL MIXER (CSM).
- A LEVEL PLATFORM SHALL BE PROVIDED FOR THE CSM TO ENSURE VERTICALITY.
- THE FINAL DESIGN MIX SHOULD BE DETERMINED BY SUITABILITY TESTS PRIOR TO CONSTRUCTION SHEAR STRENGTH REQUIREMENTS.
- THE CONSTRUCTION OF THE CUT-OFF WALL SHALL BE SUPERVISED BY A QUALIFIED GEOTECHNICAL ENGINEER.

1. CONSTRUCTION METHOD ASSUMED TO BE CUTTER SOIL MIXER (CSM).

2. A LEVEL PLATFORM SHALL BE PROVIDED FOR THE CSM TO ENSURE VERTICALITY.

3. THE FINAL DESIGN MIX SHOULD BE DETERMINED BY SUITABILITY TESTS PRIOR TO CONSTRUCTION SHEAR STRENGTH REQUIREMENTS.

4. THE CONSTRUCTION OF THE CUT-OFF WALL SHALL BE SUPERVISED BY A QUALIFIED GEOTECHNICAL ENGINEER.

Foth Infrastructure & Environment, LLC		BACK FORTY PROJECT	
REVISED DATE BY	DESCRIPTION	REVISED DATE BY	DESCRIPTION

FIGURE 4 TYPICAL CUT-OFF WALL SECTION DETAIL STEPHENSON, MICHIGAN	
PREPARED BY:	MJV/2
REVIEWED BY:	DRD
APPROVED BY:	KKB

Project No.: 17A021  
Date: SEPTEMBER 2017  
Drafted By: JOW  
AS SHOWN



**Attachment 1**  
**Boring Logs**

PROJECT: 10-1183-0030

## RECORD OF Borehole: GB-01

SHEET 1 OF 2

LOCATION: N 5033376.66, E 454794.09

BORING DATE: AUG 3-4, 2011

DATUM:

SAMPLER HAMMER, 64kg, DROP, 750mm

PENETRATION TEST HAMMER, 64kg, DROP, 700mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWES 3m				HYDRAULIC CONDUCTIVITY, K, CM/H				ADDITIONAL LAB TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA/PILOT		ELEV. DEPTH (m)	NUMBER	TYPE	BLOWES, 3m	SHEAR STRENGTH CBR, KPA	mm V. + D mm V. - D U - D	10 <sup>3</sup>	10 <sup>4</sup>	10 <sup>5</sup>		
0	GROUND SURFACE	Loamy brown, SAND, trace gravel, trace ash.			214.01										
0.00					0.00										
0.00		Compact, reddish brown, silty SAND, some gravel, some clay.			214.00										
0.00					0.00										
0.00		Compact, blackish-brown, angular GRAVEL and COBBLES.			213.98										
0.00					0.00										
0.00		Very dense, reddish-brown, SAND and GRAVEL, some silt, trace to some clay.			213.96										
0.00					0.00										
0.00		CONTINUED NEXT PAGE													

G74-BH5031-10-1183-0030.CPJ.CAL.MIS.D03 X 101811 ET

DEPTH SCALE:  
1:50LOGGED: ES  
CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Borehole: GB-01

SHEET 2 OF 2

LOCATION: N 5033376.65; E 434794.09

BORING DATE: AUG 3-4, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cms				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION			
		DESCRIPTION	STRATA PLOT		ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	20	60	80	10 <sup>6</sup>	10 <sup>4</sup>	10 <sup>-3</sup>	10 <sup>-2</sup>		
20	152 mm POWER AUGER	... CONTINUED FROM PREVIOUS PAGE ... Very dense, reddish-brown, SAND and GRAVEL, some silt, trace to some clay			202.73												
11					11.30												
END OF HOLE																	
12																	
13																	
14																	
15																	
16																	
17																	
18																	
19																	
20																	

GTA-RHS-001 10-1193-0003.GPJ GAL.MIS.GDT 10/18/11 ET

DEPTH SCALE

1:50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Borehole: GB-02

SHEET 1 OF 2

LOCATION: N 5033435.02; E 434804.80

BORING DATE: AUG 6-8, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BOREHOLE METHOD	SOIL PROFILE DESCRIPTION	STRAT PLOT	ELEV. DEPTH (m)	SAMPLES NUMBER	TYPE	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, K, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
							20	40	60	80	10 <sup>-5</sup>	10 <sup>-4</sup>	10 <sup>-3</sup>	10 <sup>-2</sup>			
							SHEAR STRENGTH Cv, kPa	Int. V. + rem. V. @	Q -	U - C	Wp	W	Wt	WI			
0		GROUND SURFACE Loose, brown, SAND		214.00 0.00													
1					1	DO											
2					2	DO											
3																	
4																	
5	162 mm POWER AUGER																
6	108 mm I.D. HOLLOW STEM BORING																
7		Compact, brown, SAND, some gravel, trace to some silt to SAND and GRAVEL, trace silt		208.42 6.58	4	DO										M	
8					5	DO											
9					6	DO											
10					7	DO											
		CONTINUED NEXT PAGE															

GTA-BHS 001 10-1193-0003.GPJ GAL-MIS.GDT 10/18/11 ET

DEPTH SCALE

1:50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0903

## RECORD OF Borehole: GB-02

SHEET 2 OF 2

LOCATION: N 5033436.02; E 434804.80

BORING DATE: AUG 6-8, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, K, cm/s				ADDITIONAL LAB TESTING	PIEZOMETER OR STANDPIPE INSTALLATION				
		DESCRIPTION	STRATA PLOT		ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	20	40	60	80	10 <sup>-3</sup>	10 <sup>-4</sup>	10 <sup>-5</sup>	10 <sup>-6</sup>		
					Cu, kPa	nat V. + rem V. @ U - O	Wp	Vf	10	20	30	40						
10	— CONTINUED FROM PREVIOUS PAGE ...	Compact, brown, SAND, some gravel, trace to some silt to SAND and GRAVEL, trace silt																
11	152 mm POWER AUGER	Very dense, brown, SAND and GRAVEL, some cobbles	203.85 11.13		7	DO		17										
12	ROTARY DRILL	Very dense, light brown, SAND with SILT, trace to some clay	200.50 14.46		9	DO	>100										MH	
13	76 mm CAVING BORING	Very dense, brown, SAND and GRAVEL, some cobbles	199.13 13.85		10	DO		64										
14			197.51 12.47		11	DO	>100											
15		END OF HOLE																
16																		
17																		
18																		
19																		
20																		

GTA-SHS-001 10-1193-0003.GPJ GAL-MIS.GDT 10/18/11 ET

DEPTH SCALE  
1 : 50LOGGED: ES  
CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Borehole: GB-03

SHEET 1 OF 2

LOCATION: N 5033516.78; E 434844.79

BORING DATE: AUG 11-12, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BOREHOLE METHOD	SOIL PROFILE DESCRIPTION	STRATA PLOT ELEV. DEPTH (m)	SAMPLES NUMBER	TYPE	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m 20 40 60 80 C <sub>s</sub> , kPa	HYDRAULIC CONDUCTIVITY, K, cm/s 10 <sup>-4</sup> 10 <sup>-3</sup> 10 <sup>-2</sup>	WATER CONTENT PERCENT W <sub>a</sub> 10 20 30 40 W <sub>f</sub>	ADDITIONAL LAB TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
0		GROUND SURFACE	216.37 0.00								
1		Loose, brown, SAND, some gravel									
2											
3											
4											
5											
6											
7		Compact to loose, brown, GRAVEL and SAND, trace to some silt	208.82 6.53	1 2 3 4 5 6 7 8 9 10	DO DO DO DO DO DO DO DO DO DO	20 40 60 80 00 00 00 00 00 00 00 00	10 <sup>-4</sup> 10 <sup>-3</sup> 10 <sup>-2</sup> W <sub>a</sub> 10 20 30 40 W <sub>f</sub>				
8											
9											
10	ROTARY DRILL	Dense to very dense, brown, SAND, trace to some silt	206.77 9.63								
CONTINUED NEXT PAGE											

GTA-BHS 001 10-1193-0003.GPJ Gal-MIS.GDT 10/12/11 ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

09/08/2011

PROJECT: 10-1193-0083

**RECORD OF Borehole: GB-03**

SHEET 2 OF 2

LOCATION: N 5033516.78 E 434844.79

BORING DATE: AUG 11-12, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

CEA FILES 001 100-11834003 GEI CAN. MSS. EDT 10/11/811 E

DEPTH SCALE  
1:60



LOGGED: ES  
CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Borehole: GB-04

SHEET 1 OF 3

LOCATION: N 6033677.28; E 434869.92

BORING DATE: AUG 15-17, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE			SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)		NUMBER	TYPE			20	40	60	80				
							SHEAR STRENGTH Cu, kPa	nat V. + rem V. @	Q - ● U - ○	Wp   W	10	20	30	40			
0		GROUND SURFACE		216.69 0.00													
		Loose, brown, SAND, some gravel															
1																	
2																	
3				212.64 3.06													
		Very loose to compact; brown, SAND, trace gravel, trace to some silt															M
4																	
5				210.66 5.03													
		Very dense, brown, SAND and GRAVEL, trace to some silt															
6																	
7		Dense to loose, brown, Silty SAND, trace to some clay to SAND, trace to some gravel, trace to some silt, trace to some clay		209.04 6.66													M
8																	
9																	
10																	
		CONTINUED NEXT PAGE															

GTA-BHS 001 10-1193-0003.GPJ, GAL-MIS.GDT, 19/18/11, ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0008

## RECORD OF Borehole: GB-04

SHEET 2 OF 3

LOCATION: N 5033577.28 ; E 434869.92

BORING DATE: AUG 15-17, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, K, cm/s				ADDITIONAL LAB TESTING	PIEZOMETER OR STANDPIPE INSTALLATION			
		DESCRIPTION	STRATA/LOT		ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	20	40	60	80	10 <sup>-8</sup>	10 <sup>-4</sup>	10 <sup>-3</sup>	10 <sup>-2</sup>	
10		... CONTINUED FROM PREVIOUS PAGE ...															
11		Dense to loose, brown, Silty SAND, trace to some clay to SAND, trace to some gravel, trace to some silt, trace to some clay			204.46	7	DO	8									
12	ROTARY DRILL	Very dense, brown, Silty SAND, trace gravel, trace to some clay				8	DO	60									24H
13		162 mm CASING ADVANCE 30082011				9	DO	91									
14						10	DO	71									
15						11	DO	83									
16						12	DO	>100									M
17	ROTARY DRILL				197.61												
18		NO CORE 30082011			17.98												M
19																	
20		Very dense, brown, SAND and GRAVEL, trace to some silt, trace to some clay															

CONTINUED NEXT PAGE

GTA-BHS 006 10-1193-0008.GPL1 GAL-MIS.GDT 10/18/11 ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Borehole: GB-04

SHEET 3 OF 3

LOCATION: N 5033577.28; E 434869.82

BORING DATE: AUG 15-17, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, K, cm/s				PIEZOMETER OR STANDPIPE INSTALLATION				
		DESCRIPTION	STRATA PT.CT		ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	20	40	60	80	$10^{-6}$	$10^{-4}$	$10^{-2}$	$10^0$	
									SHEAR STRENGTH Cu, kPa	nat V. + rem V. $\oplus$	Q - $\bullet$ U - O	Wp $\downarrow$ $\ominus$	W $\downarrow$ $\ominus$	Wf $\downarrow$ $\ominus$			
20	ROTARY DRILL, NO CORE RECORDED	— CONTINUED FROM PREVIOUS PAGE — Very dense, brown, SAND and GRAVEL, trace to some silt, trace to some clay			194.69												
21		END OF HOLE			20.90												
22																	
23																	
24																	
25																	
26																	
27																	
28																	
29																	
30																	

GTA-SHS-001 10-1193-0003.GPJ GAL MS.GDT 10/18/11 ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

PROJECT: 10-1183-0003

## RECORD OF Borehole: GB-05

SHEET 1 OF 2

LOCATION: N 5033620.44, E 434845.71

BORING DATE: AUG 19-20, 2011

DATUM:

SAMPLER HAMMER, 64kg, DROP, 760mm

PENETRATION TEST HAMMER, 64kg, DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, K, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
					20	40	60	80	10 <sup>-4</sup>	10 <sup>-5</sup>	10 <sup>-6</sup>	10 <sup>-7</sup>			
		STRATA PLOT	ELEV. DEPTH (m)		NUMBER	TYPE	BLOWSG/0.3m	SHEAR STRENGTH Cu, kPa	nat V. + rem V. ⊕	Q - ● U - ○	W <sub>p</sub>	W	W <sub>i</sub>		
0	GROUND SURFACE		214.27 0.00		1	DO	28								
0.5	Compact, brown, Silty SAND, some gravel, trace clay														
1															
2															
3	Compact, brown, SAND, some gravel, trace to some clay		213.84 2.44		2	DO	29								
4					3	DO	12								
5					4	DO	60								
6					5	DO	68								
7	Very dense, SAND and GRAVEL, trace to some silt, trace to some clay		207.87 6.40		6	DO	53							M	18/08/2011
8															
9															
10															

CONTINUED NEXT PAGE

GTA-SHS-001 10-1183-0003.GPR GAL-MIS.GDT 10/16/11 ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Borehole: GB-05

SHEET 2 OF 2

LOCATION: N 5033620.44 ; E 434945.71

BORING DATE: AUG 19-20, 2011

DATUM:

SAMPLER HAMMER, 64kg; DROP, 760mm

PENETRATION TEST HAMMER, 64kg; DROP, 760mm

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES	DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, K. cm/s				ADDITIONAL LAB TESTING	PIEZOMETER OR STANDPIPE INSTALLATION			
		DESCRIPTION	STRATA PLOT		ELEV. DEPTH (m)	NUMBER	TYPE	20	40	60	80	10 <sup>4</sup>	10 <sup>4</sup>	10 <sup>4</sup>	10 <sup>-2</sup>		
					20	40	60	80	U, kPa	nat V. + rem V. $\oplus$	Q - C	U - C	W <sub>p</sub>	W	W <sub>t</sub>		
10	ROTARY DRILL	— CONTINUED FROM PREVIOUS PAGE — Very dense, SAND and GRAVEL, trace to some silt, trace to some clay															
11	100 mm CASING ADVANCED 18/8/2011				202.62	7	DO	80									
12		END OF HOLE			11.65												
13																	
14																	
15																	
16																	
17																	
18																	
19																	
20																	

GTA-BHS 001 10-1193-0003.GPJ Gal-MIS.GDT 10/18/11 ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

**RECORD OF Drillhole: GB-01**

SHEET 1 OF 2

LOCATION: N 5033376.7 ; E 434794.1

DRILLING DATE: AUG 3-4, 2011

## DATUM

INCLINATION: -90°      AZIMUTH: —

DRAIL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

CONTINUED NEXT PAGE



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

**RECORD OF Drillhole: GB-01**

SHEET 2 OF 2

LOCATION: N 5033376.7 E 434794.1

DRILLING DATE: AUG 34, 2011

DATUM:

INCLINATION: -90°      AZIMUTH: -45°

DRILL RIG: D-120

## DRILLING CONTR

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE: E

七



LOGGED: ES

CHECKED:

EPA-R5-2018-009055 0000373 0026

PROJECT: 10-1193-0003

## RECORD OF Drillhole: GB-02

SHEET 1 OF 2

LOCATION: N 5033435.0 E 434804.8

DRILLING DATE: AUG 6-8, 2011

DATUM:

INCINATION: -90° AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. DEPTH (m)	RIN NO.	FLUSH/RETURN	JN - Joint FLT - Fault SHR - Shear VN - Vein CR - Orthogonal CJ - Conjugate	BD - Bedding FO - Foliation CO - Contact OR - Orthogonal CL - Cleavage	PL - Planar CU - Curved UN - Undulose ST - Stepped IR - Irregular	PO - Polished X - Backsided SM - Smooth RO - Rough MB - Mechanical Break	BR - Broken Rock NOTE: For additional information refer to Box of abbreviations & symbols.	HYDRAULIC CONDUCTIVITY K, cm/sec	WEAKENING INDEX	FEATURES	NOTES	
		Continued from Record of Borehole GB-02		197.51												
17		17.47 - 25.55 m Slightly weathered, massive to moderately foliated, very light to medium light grey and yellowish grey, fine to medium grained, non to faintly porous, weak to medium strong RHYOLITE CRYSTAL TUFF (RCTF), abundant quartz eyes, generally lacking iron oxidation -Moderate silicification, weak to moderate sericitic alteration -Trace disseminated very fine grained pyrite throughout interval		17.47												
18					1											
19																
20																
21																
22																
23																
24																
25																
26																
27		26.56 - 27.67 m Slightly weathered, massive to foliated, light bluish grey to pinkish grey, fine to medium grained, highly porous with pitted texture, weak to medium strong RHYOLITE CRYSTAL TUFF (RCTF)		26.55												
		CONTINUED NEXT PAGE														

GIA-ROCK 036 10-1193-0003 GPU GAL-MISS.GDT S2/S11 ET

DEPTH SCALE

1 : 50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Drillhole: GB-02

SHEET 2 OF 2

LOCATION: N 6033436.0 ; E 434804.8

DRILLING DATE: AUG 6-8, 2011

DATUM:

INCLINATION: -90° AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. (m)	RUN NO.	FLUSH RETURN	RECOVERY	TOTAL CORE % SOLID	R.O.D. % PER meter	FRACTION PER meter	DP w/w core length	DISCONTINUITY DATA	TYPE AND SURFACE DESCRIPTION	HYDRAULIC CONDUCTIVITY K, cm/sec	WEATHERING INDEX	FEATURES	NOTES	
													JN - Joint	BD - Bedding	PL - Planar	PO - Polished	BR - Broken Rock	
F2,F - Fault	FO - Foliation	CU - Curved	K - Smooth															NOTE: Use additional symbols if required to describe intersections & symbols.
VN - Vein	GR - Orthogonal	ST - Stepped	Ro - Rough															
CJ - Conjugate	CL - Cleavage	IR - Irregular	MB - Mechanical Break															
<b>-- CONTINUED FROM PREVIOUS PAGE --</b>																		
28		27.67 - 31.02 m Slightly weathered to fresh, massive, very light grey to dark grey, fine to coarse grained, faintly porous, medium strong RHYOLITE CRYSTAL TUFF (RCTF)		187.30 27.68	9								JN,PL,VR					
29													JN,PL,VR					
30													JN,PL,RO					
31	NO-3 BB / ING Rods Trial True Sampling	31.02 - 33.55 m: Fresh, bedded, light bluish grey to medium grey, fine to medium grained, non-porous, medium strong TUFACEOUS SEDIMENTS (TFSD) -Moderate silification -Some pale yellow irregular siliceous veinlets		183.98 31.02	11								JN,PL,RO JN,PL,RO,SA					
32													JN,PL,SM JN,PL,SM JN,PL,VR,ST SH,PL,VR JN,PL,RO					
33													JN,PL,SM,OX,ST FO,PL,SM FO,PL,RO					
34		33.55 - 34.87 m Fresh, foliated, greyish black and moderate olive brown, fine to medium grained, faintly to moderately porous, medium strong, MASSIVE SULPHIDE (MASU), containing sub-hedral, fine grained pyrite with sphalerite in slightly dipping, undulating bands -Slightly brecciated texture and randomly oriented micro-defects		181.43 33.55	12								FO,PL,RO FO,PL,RO CO,PL,VR SH,PL,RO					
35		END OF DRILLHOLE		180.11 34.87	13								VN,PL,VR VN,PL,VR VN,PL,VR VN,PL,RO VN,PL,SM					
36																		
37																		

GYA-RCK 030 10-1193-0003.GP4 GALMISS.GDT 8/29/11 ET

DEPTH SCALE

1:50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Drillhole: GB-03

SHEET 1 OF 3

LOCATION: N 5033616.8 ; E 434844.8

DRILLING DATE: AUG 11-12, 2011

DATUM:

INCLINATION: -90° AZIMUTH: ---

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. DEPTH (m)	RUN No.	FLUSH RETURN	JN - Joint FLT - Fault SHR - Shear VN - Vein CJ - Conjugate	BD - Bedding FO - Foliation CO - Contact OR - Orthogonal CL - Cleavage	PL - Plane CU - Curved UN - Unbedded ST - Stepped IR - Irregular MB - Mechanical break	PO - Polished K - Streaked SM - Smooth RO - Rough MB - Mechanical break	BR - Broken Rock	DISCONTINUITY DATA						HYDRAULIC CONDUCTIVITY K, cm/sec	WEATHERING INDEX W.E.I.	FEATURES	NOTES					
												TOTAL CORE %	SOLID CORE %	F.O.D. % Molar %	RECOVERY INDEX %	FRACK INDEX %	10 <sup>-2</sup> GROSS AXIS %	10 <sup>-2</sup> NET AXIS %	10 <sup>-2</sup> 10 <sup>-2</sup> 10 <sup>-2</sup>							
17.71		Continued from Record of Borehole GB-03		197.69																						
18		17.71 - 39.20 m Slightly to moderately weathered, massive to foliated, medium dark grey to dark reddish brown, ephemeritic to medium grained, non-porous, medium strong to strong, RHYOLITE CRYSTAL TUFF (RCTF) -Moderately silicified, medium to coarse grained quartz eyes and oxidation throughout -15% disseminated very fine grained pyrite zone from 18.17 - 18.38 m		17.71	1																					
19					2																					
20					3																					
21					4																					
22					5																					
23					6																					
24					7																					
25					8																					
26					9																					
27																										
		CONTINUED NEXT PAGE																								

PROJECT: 10-1193-0003

**RECORD OF Drillhole: GB-03**

SHEET 2 OF 3

LOCATION: N 5033516.8 ; E 434844.8

DRILLING DATE: AUG 11-12, 2011

**DATUM**

INCLINATION: -90°      AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

CONTINUED NEXT PAGE



LOGGED: ES

三

CHECKED:

PROJECT: 10-1193-0003

**RECORD OF Drillhole: GB-03**

SHEET 3 OF 3

LOCATION: N 5033516.8 ; E 434844.8

DRILLING DATE: AUG 11-12, 2011

**DATUM:**

INCLINATION: -90°      AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

61A-RECK 030 18-11293-0003 SP23 GAI-MISS GPT 9/29/11 ET

**DEPTH SCALE**

1:50



LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

## RECORD OF Drillhole: GB-04

SHEET 1 OF 3

LOCATION: N 6033577.3, E 434869.9

DRILLING DATE: AUG 15-17, 2011

DATUM:

INCLINATION: -90° AZIMUTH: ---

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. (m)	RUN NO.	FLUSH RETURNS	JN - Joint			BD - Bedding	PL - Planar	PO - Potholed	BR - Broken Rock	NOTE: For additional abbreviations refer to list of symbols & symbols.	FEATURES	NOTES
							RECOVERY %	R.O.D. %	FRACTURE INDEX							
							TOTAL CORE %	SOLID CORE %	PSR Molar	DPW/1 CORE LBS	JF 10 15 20 30	N1 N2 N3 N4 N5 N6				
		Continued from Record of Borehole GB-04		194.00												
21		20.90 - 21.85 m Highly weathered, massive, white chalky, fine grained, highly porous, very weak to weak RHYOLITE CRYSTAL TUFF (RCTF)		180.00	2						JN, PL, VR, ST, OX					Bc
				193.74							JN, PL, RO, ST, OX					Lc
22		21.85 - 24.50 m Moderately weathered, foliated, pinkish grey to dark reddish brown, aphanitic to medium grained, faintly porous, occasional vugs, weak to medium strong RHYOLITE CRYSTAL TUFF (RCTF) -Moderately silicified and highly oxidized on almost all joint surfaces		21.05	3						SH, PL, PO					
				191.00							JN, PL, RO, IN, SA, NM					
23				24.50							JN, PL, RO, SA, OX, CA					
				191.00							JN, PL, VR, SA, OX, CA					
24				24.50							JN, PL, VR, SA, OX, CA					
				191.00							JN, PL, SM, SA, OX, CA					
25		24.50 - 26.07 m Moderately weathered, foliated, medium dark grey, fine to medium grained, non-porous, strong, RHYOLITE CRYSTAL TUFF (RCTF) -Darker grey, harder, strongly silicified zone between 25.00 - 26.00 m -Trace fine grained pyrite throughout		24.50	4						JN, PL, RO, CT, CL, CM					
				188.72							JN, PL, RO, ST, CL					
26				24.57							JN, PL, SM					
				191.00							JN, PL, SM, CT, CL					
27		26.07 - 30.42 m Moderately weathered, foliated, pinkish grey to dark reddish brown, aphanitic to medium grained, faintly porous, weak to medium strong, RHYOLITE CRYSTAL TUFF (RCTF) -Slight silification and sericitic alteration		24.57	5						JN, PL, SM, SA, OX, CA					
				188.72							JN, PL, RO					
28				24.57							JN, PL, RO, ST, OX					
				188.72							JN, PL, SM, SA, OX, CA					
29				24.57							JN, PL, RO, IN, CL					
				188.72							JN, PL, RO, ST, OX					
30				24.57							JN, PL, SM, SA, OX, CA					
				188.72							JN, PL, RO, SA, OX, SA					
31				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
32				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
33				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
34				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
35				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
36				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
37				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
38				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
39				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
40				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
41				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
42				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
43				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
44				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
45				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
46				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
47				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
48				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
49				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
50				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
51				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
52				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
53				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
54				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
55				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
56				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
57				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
58				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
59				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
60				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
61				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
62				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
63				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
64				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
65				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
66				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
67				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
68				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
69				24.57							SH, PL, RO, ST, OX, OX, CL					
				188.72							JN, PL, RO, 8A, OX, SA					
70</																

PROJECT: 10-1193-0003

LOCATION: N 5033577.3, E 434869.9

INCLINATION: -90° AZIMUTH: --

## RECORD OF Drillhole: GB-04

SHEET 2 OF 3

DRILLING DATE: AUG 16-17, 2011

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DATUM:

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. (m)	RUN No.	FLUSH RETURN	TOTAL CORE % 88.9%	SOILS CORE % 23.9%	R.G.D. %	FRACT. INDEX PERC Molar W/VIN	BD - Bedding FO - Foliation CO - Contact OK - Orthogonal CI - Cleavage	PL - Planar CS - Curved UK - Undulating ST - Stippled IR - Irregular	PO - Pollenoid K - Stickenstedt SM - Smith Ro - Rough MB - Mechanical Break	BR - Broken Rock	NOTE: For additional abbreviations refer to the list of symbols & acronyms	HYDRAULIC CONDUCTIVITY K, cm/sec	WEATH- ERING INDEX	FEATURES	NOTES	
<b>... CONTINUED FROM PREVIOUS PAGE ...</b>																				
31		30.42 - 32.30 m Slightly weathered, highly foliated, medium dark grey and dark red, fine to medium grained, non-porous, medium strong to strong, RHYOLITE CRYSTAL TUFF (RCTF) -Highly silicified, slight sericitic/chlorite alteration -Trace disseminated very fine grained pyrite from 30.50 - 32.30 m			9															
32		32.30 - 41.24 m Slightly weathered, weakly foliated, light grey with dark green grains, fine to coarse grained, non-porous, medium strong to strong, RHYOLITE CRYSTAL TUFF (RCTF) -Moderately silicified, slight sericitic/chlorite alteration -Trace disseminated very fine grained pyrite		183.29 32.30	10															
33																				
34					11															
35					12															
36					13															
37					14															
38					15															
CONTINUED NEXT PAGE																				
GALMISS GDT 9/26/11 ET										Golder Associates										
DEPTH SCALE 1:50										LOGGED: ES CHECKED:										

PROJECT: 10-1193-0003

## RECORD OF Drillhole: GB-04

SHEET 3 OF 3

LOCATION: N 5033577.3 ;E 434869.9

DRILLING DATE: AUG 16-17, 2011

DATUM:

INCLINATION: -90° AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. DEPTH (m)	KJN No.	PUSH/RETURN	JN - Joint		BD - Bedding		PL - Planar		PO - Polished		BR - Broken Rock		NOTES
FLT - Flat	SHR - Shear	CO - Contact	UN - Undulating	CU - Curved	ST - Stepped	IR - Irregular	GR - Geological	SM - Smooth	Ro - Rough	MZ - Mechanical Break	BR - Brittle						
							TOTAL DEPTH %	SOLID CONE %	R.D.D.	FRACT. INDEX	DIP w.t. PER. METER	TYPE AND SURFACE DESCRIPTION	LAMINARIC CONDUCTIVITY K CONDUCTIVE	10<sup>-6</sup> 10<sup>-7</sup> 10<sup>-8</sup> 10<sup>-9</sup> 10<sup>-10</sup> 10<sup>-11</sup> 10<sup>-12</sup> 10<sup>-13</sup> 10<sup>-14</sup> 10<sup>-15</sup> 10<sup>-16</sup> 10<sup>-17</sup> 10<sup>-18</sup> 10<sup>-19</sup> 10<sup>-20</sup> 10<sup>-21</sup> 10<sup>-22</sup> 10<sup>-23</sup> 10<sup>-24</sup> 10<sup>-25</sup> 10<sup>-26</sup> 10<sup>-27</sup> 10<sup>-28</sup> 10<sup>-29</sup> 10<sup>-30</sup> 10<sup>-31</sup> 10<sup>-32</sup> 10<sup>-33</sup> 10<sup>-34</sup> 10<sup>-35</sup> 10<sup>-36</sup> 10<sup>-37</sup> 10<sup>-38</sup> 10<sup>-39</sup> 10<sup>-40</sup> 10<sup>-41</sup> 10<sup>-42</sup> 10<sup>-43</sup> 10<sup>-44</sup> 10<sup>-45</sup> 10<sup>-46</sup> 10<sup>-47</sup> 10<sup>-48</sup> 10<sup>-49</sup> 10<sup>-50</sup> 10<sup>-51</sup> 10<sup>-52</sup> 10<sup>-53</sup> 10<sup>-54</sup> 10<sup>-55</sup> 10<sup>-56</sup> 10<sup>-57</sup> 10<sup>-58</sup> 10<sup>-59</sup> 10<sup>-60</sup> 10<sup>-61</sup> 10<sup>-62</sup> 10<sup>-63</sup> 10<sup>-64</sup> 10<sup>-65</sup> 10<sup>-66</sup> 10<sup>-67</sup> 10<sup>-68</sup> 10<sup>-69</sup> 10<sup>-70</sup> 10<sup>-71</sup> 10<sup>-72</sup> 10<sup>-73</sup> 10<sup>-74</sup> 10<sup>-75</sup> 10<sup>-76</sup> 10<sup>-77</sup> 10<sup>-78</sup> 10<sup>-79</sup> 10<sup>-80</sup> 10<sup>-81</sup> 10<sup>-82</sup> 10<sup>-83</sup> 10<sup>-84</sup> 10<sup>-85</sup> 10<sup>-86</sup> 10<sup>-87</sup> 10<sup>-88</sup> 10<sup>-89</sup> 10<sup>-90</sup> 10<sup>-91</sup> 10<sup>-92</sup> 10<sup>-93</sup> 10<sup>-94</sup> 10<sup>-95</sup> 10<sup>-96</sup> 10<sup>-97</sup> 10<sup>-98</sup> 10<sup>-99</sup> 10<sup>-100</sup> 10<sup>-101</sup> 10<sup>-102</sup> 10<sup>-103</sup> 10<sup>-104</sup> 10<sup>-105</sup> 10<sup>-106</sup> 10<sup>-107</sup> 10<sup>-108</sup> 10<sup>-109</sup> 10<sup>-110</sup> 10<sup>-111</sup> 10<sup>-112</sup> 10<sup>-113</sup> 10<sup>-114</sup> 10<sup>-115</sup> 10<sup>-116</sup> 10<sup>-117</sup> 10<sup>-118</sup> 10<sup>-119</sup> 10<sup>-120</sup> 10<sup>-121</sup> 10<sup>-122</sup> 10<sup>-123</sup> 10<sup>-124</sup> 10<sup>-125</sup> 10<sup>-126</sup> 10<sup>-127</sup> 10<sup>-128</sup> 10<sup>-129</sup> 10<sup>-130</sup> 10<sup>-131</sup> 10<sup>-132</sup> 10<sup>-133</sup> 10<sup>-134</sup> 10<sup>-135</sup> 10<sup>-136</sup> 10<sup>-137</sup> 10<sup>-138</sup> 10<sup>-139</sup> 10<sup>-140</sup> 10<sup>-141</sup> 10<sup>-142</sup> 10<sup>-143</sup> 10<sup>-144</sup> 10<sup>-145</sup> 10<sup>-146</sup> 10<sup>-147</sup> 10<sup>-148</sup> 10<sup>-149</sup> 10<sup>-150</sup> 10<sup>-151</sup> 10<sup>-152</sup> 10<sup>-153</sup> 10<sup>-154</sup> 10<sup>-155</sup> 10<sup>-156</sup> 10<sup>-157</sup> 10<sup>-158</sup> 10<sup>-159</sup> 10<sup>-160</sup> 10<sup>-161</sup> 10<sup>-162</sup> 10<sup>-163</sup> 10<sup>-164</sup> 10<sup>-165</sup> 10<sup>-166</sup> 10<sup>-167</sup> 10<sup>-168</sup> 10<sup>-169</sup> 10<sup>-170</sup> 10<sup>-171</sup> 10<sup>-172</sup> 10<sup>-173</sup> 10<sup>-174</sup> 10<sup>-175</sup> 10<sup>-176</sup> 10<sup>-177</sup> 10<sup>-178</sup> 10<sup>-179</sup> 10<sup>-180</sup> 10<sup>-181</sup> 10<sup>-182</sup> 10<sup>-183</sup> 10<sup>-184</sup> 10<sup>-185</sup> 10<sup>-186</sup> 10<sup>-187</sup> 10<sup>-188</sup> 10<sup>-189</sup> 10<sup>-190</sup> 10<sup>-191</sup> 10<sup>-192</sup> 10<sup>-193</sup> 10<sup>-194</sup> 10<sup>-195</sup> 10<sup>-196</sup> 10<sup>-197</sup> 10<sup>-198</sup> 10<sup>-199</sup> 10<sup>-200</sup> 10<sup>-201</sup> 10<sup>-202</sup> 10<sup>-203</sup> 10<sup>-204</sup> 10<sup>-205</sup> 10<sup>-206</sup> 10<sup>-207</sup> 10<sup>-208</sup> 10<sup>-209</sup> 10<sup>-210</sup> 10<sup>-211</sup> 10<sup>-212</sup> 10<sup>-213</sup> 10<sup>-214</sup> 10<sup>-215</sup> 10<sup>-216</sup> 10<sup>-217</sup> 10<sup>-218</sup> 10<sup>-219</sup> 10<sup>-220</sup> 10<sup>-221</sup> 10<sup>-222</sup> 10<sup>-223</sup> 10<sup>-224</sup> 10<sup>-225</sup> 10<sup>-226</sup> 10<sup>-227</sup> 10<sup>-228</sup> 10<sup>-229</sup> 10<sup>-230</sup> 10<sup>-231</sup> 10<sup>-232</sup> 10<sup>-233</sup> 10<sup>-234</sup> 10<sup>-235</sup> 10<sup>-236</sup> 10<sup>-237</sup> 10<sup>-238</sup> 10<sup>-239</sup> 10<sup>-240</sup> 10<sup>-241</sup> 10<sup>-242</sup> 10<sup>-243</sup> 10<sup>-244</sup> 10<sup>-245</sup> 10<sup>-246</sup> 10<sup>-247</sup> 10<sup>-248</sup> 10<sup>-249</sup> 10<sup>-250</sup> 10<sup>-251</sup> 10<sup>-252</sup> 10<sup>-253</sup> 10<sup>-254</sup> 10<sup>-255</sup> 10<sup>-256</sup> 10<sup>-257</sup> 10<sup>-258</sup> 10<sup>-259</sup> 10<sup>-260</sup> 10<sup>-261</sup> 10<sup>-262</sup> 10<sup>-263</sup> 10<sup>-264</sup> 10<sup>-265</sup> 10<sup>-266</sup> 10<sup>-267</sup> 10<sup>-268</sup> 10<sup>-269</sup> 10<sup>-270</sup> 10<sup>-271</sup> 10<sup>-272</sup> 10<sup>-273</sup> 10<sup>-274</sup> 10<sup>-275</sup> 10<sup>-276</sup> 10<sup>-277</sup> 10<sup>-278</sup> 10<sup>-279</sup> 10<sup>-280</sup> 10<sup>-281</sup> 10<sup>-282</sup> 10<sup>-283</sup> 10<sup>-284</sup> 10<sup>-285</sup> 10<sup>-286</sup> 10<sup>-287</sup> 10<sup>-288</sup> 10<sup>-289</sup> 10<sup>-290</sup> 10<sup>-291</sup> 10<sup>-292</sup> 10<sup>-293</sup> 10<sup>-294</sup> 10<sup>-295</sup> 10<sup>-296</sup> 10<sup>-297</sup> 10<sup>-298</sup> 10<sup>-299</sup> 10<sup>-300</sup> 10<sup>-301</sup> 10<sup>-302</sup> 10<sup>-303</sup> 10<sup>-304</sup> 10<sup>-305</sup> 10<sup>-306</sup> 10<sup>-307</sup> 10<sup>-308</sup> 10<sup>-309</sup> 10<sup>-310</sup> 10<sup>-311</sup> 10<sup>-312</sup> 10<sup>-313</sup> 10<sup>-314</sup> 10<sup>-315</sup> 10<sup>-316</sup> 10<sup>-317</sup> 10<sup>-318</sup> 10<sup>-319</sup> 10<sup>-320</sup> 10<sup>-321</sup> 10<sup>-322</sup> 10<sup>-323</sup> 10<sup>-324</sup> 10<sup>-325</sup> 10<sup>-326</sup> 10<sup>-327</sup> 10<sup>-328</sup> 10<sup>-329</sup> 10<sup>-330</sup> 10<sup>-331</sup> 10<sup>-332</sup> 10<sup>-333</sup> 10<sup>-334</sup> 10<sup>-335</sup> 10<sup>-336</sup> 10<sup>-337</sup> 10<sup>-338</sup> 10<sup>-339</sup> 10<sup>-340</sup> 10<sup>-341</sup> 10<sup>-342</sup> 10<sup>-343</sup> 10<sup>-344</sup> 10<sup>-345</sup> 10<sup>-346</sup> 10<sup>-347</sup> 10<sup>-348</sup> 10<sup>-349</sup> 10<sup>-350</sup> 10<sup>-351</sup> 10<sup>-352</sup> 10<sup>-353</sup> 10<sup>-354</sup> 10<sup>-355</sup> 10<sup>-356</sup> 10<sup>-357</sup> 10<sup>-358</sup> 10<sup>-359</sup> 10<sup>-360</sup> 10<sup>-361</sup> 10<sup>-362</sup> 10<sup>-363</sup> 10<sup>-364</sup> 10<sup>-365</sup> 10<sup>-366</sup> 10<sup>-367</sup> 10<sup>-368</sup> 10<sup>-369</sup> 10<sup>-370</sup> 10<sup>-371</sup> 10<sup>-372</sup> 10<sup>-373</sup> 10<sup>-374</sup> 10<sup>-375</sup> 10<sup>-376</sup> 10<sup>-377</sup> 10<sup>-378</sup> 10<sup>-379</sup> 10<sup>-380</sup> 10<sup>-381</sup> 10<sup>-382</sup> 10<sup>-383</sup> 10<sup>-384</sup> 10<sup>-385</sup> 10<sup>-386</sup> 10<sup>-387</sup> 10<sup>-388</sup> 10<sup>-389</sup> 10<sup>-390</sup> 10<sup>-391</sup> 10<sup>-392</sup> 10<sup>-393</sup> 10<sup>-394</sup> 10<sup>-395</sup> 10<sup>-396</sup> 10<sup>-397</sup> 10<sup>-398</sup> 10<sup>-399</sup> 10<sup>-400</sup> 10<sup>-401</sup> 10<sup>-402</sup> 10<sup>-403</sup> 10<sup>-404</sup> 10<sup>-405</sup> 10<sup>-406</sup> 10<sup>-407</sup> 10<sup>-408</sup> 10<sup>-409</sup> 10<sup>-410</sup> 10<sup>-411</sup> 10<sup>-412</sup> 10<sup>-413</sup> 10<sup>-414</sup> 10<sup>-415</sup> 10<sup>-416</sup> 10<sup>-417</sup> 10<sup>-418</sup> 10<sup>-419</sup> 10<sup>-420</sup> 10<sup>-421</sup> 10<sup>-422</sup> 10<sup>-423</sup> 10<sup>-424</sup> 10<sup>-425</sup> 10<sup>-426</sup> 10<sup>-427</sup> 10<sup>-428</sup> 10<sup>-429</sup> 10<sup>-430</sup> 10<sup>-431</sup> 10<sup>-432</sup> 10<sup>-433</sup> 10<sup>-434</sup> 10<sup>-435</sup> 10<sup>-436</sup> 10<sup>-437</sup> 10<sup>-438</sup> 10<sup>-439</sup> 10<sup>-440</sup> 10<sup>-441</sup> 10<sup>-442</sup> 10<sup>-443</sup> 10<sup>-444</sup> 10<sup>-445</sup> 10<sup>-446</sup> 10<sup>-447</sup> 10<sup>-448</sup> 10<sup>-449</sup> 10<sup>-450</sup> 10<sup>-451</sup> 10<sup>-452</sup> 10<sup>-453</sup> 10<sup>-454</sup> 10<sup>-455</sup> 10<sup>-456</sup> 10<sup>-457</sup> 10<sup>-458</sup> 10<sup>-459</sup> 10<sup>-460</sup> 10<sup>-461</sup> 10<sup>-462</sup> 10<sup>-463</sup> 10<sup>-464</sup> 10<sup>-465</sup> 10<sup>-466</sup> 10<sup>-467</sup> 10<sup>-468</sup> 10<sup>-469</sup> 10<sup>-470</sup> 10<sup>-471</sup> 10<sup>-472</sup> 10<sup>-473</sup> 10<sup>-474</sup> 10<sup>-475</sup> 10<sup>-476</sup> 10<sup>-477</sup> 10<sup>-478</sup> 10<sup>-479</sup> 10<sup>-480</sup> 10<sup>-481</sup> 10<sup>-482</sup> 10<sup>-483</sup> 10<sup>-484</sup> 10<sup>-485</sup> 10<sup>-486</sup> 10<sup>-487</sup> 10<sup>-488</sup> 10<sup>-489</sup> 10<sup>-490</sup> 10<sup>-491</sup> 10<sup>-492</sup> 10<sup>-493</sup> 10<sup>-494</sup> 10<sup>-495</sup> 10<sup>-496</sup> 10<sup>-497</sup> 10<sup>-498</sup> 10<sup>-499</sup> 10<sup>-500</sup> 10<sup>-501</sup> 10<sup>-502</sup> 10<sup>-503</sup> 10<sup>-504</sup> 10<sup>-505</sup> 10<sup>-506</sup> 10<sup>-507</sup> 10<sup>-508</sup> 10<sup>-509</sup> 10<sup>-510</sup> 10<sup>-511</sup> 10<sup>-512</sup> 10<sup>-513</sup> 10<sup>-514</sup> 10<sup>-515</sup> 10<sup>-516</sup> 10<sup>-517</sup> 10<sup>-518</sup> 10<sup>-519</sup> 10<sup>-520</sup> 10<sup>-521</sup> 10<sup>-522</sup> 10<sup>-523</sup> 10<sup>-524</sup> 10<sup>-525</sup> 10<sup>-526</sup> 10<sup>-527</sup> 10<sup>-528</sup> 10<sup>-529</sup> 10<sup>-530</sup> 10<sup>-531</sup> 10<sup>-532</sup> 10<sup>-533</sup> 10<sup>-534</sup> 10<sup>-535</sup> 10<sup>-536</sup> 10<sup>-537</sup> 10<sup>-538</sup> 10<sup>-539</sup> 10<sup>-540</sup> 10<sup>-541</sup> 10<sup>-542</sup> 10<sup>-543</sup> 10<sup>-544</sup> 10<sup>-545</sup> 10<sup>-546</sup> 10<sup>-547</sup> 10<sup>-548</sup> 10<sup>-549</sup> 10<sup>-550</sup> 10<sup>-551</sup> 10<sup>-552</sup> 10<sup>-553</sup> 10<sup>-554</sup> 10<sup>-555</sup> 10<sup>-556</sup> 10<sup>-557</sup> 10<sup>-558</sup> 10<sup>-559</sup> 10<sup>-560</sup> 10<sup>-561</sup> 10<sup>-562</sup> 10<sup>-563</sup> 10<sup>-564</sup> 10<sup>-565</sup> 10<sup>-566</sup> 10<sup>-567</sup> 10<sup>-568</sup> 10<sup>-569</sup> 10<sup>-570</sup> 10<sup>-571</sup> 10<sup>-572</sup> 10<sup>-573</sup> 10<sup>-574</sup> 10<sup>-575</sup> 10<sup>-576</sup> 10<sup>-577</sup> 10<sup>-578</sup> 10<sup>-579</sup> 10<sup>-580</sup> 10<sup>-581</sup> 10<sup>-582</sup> 10<sup>-583</sup> 10<sup>-584</sup> 10<sup>-585</sup> 10<sup>-586</sup> 10<sup>-587</sup> 10<sup>-588</sup> 10<sup>-589</sup> 10<sup>-590</sup> 10<sup>-591</sup> 10<sup>-592</sup> 10<sup>-593</sup> 10<sup>-594</sup> 10<sup>-595</sup> 10<sup>-596</sup> 10<sup>-597</sup> 10<sup>-598</sup> 10<sup>-599</sup> 10<sup>-600</sup> 10<sup>-601</sup> 10<sup>-602</sup> 10<sup>-603</sup> 10<sup>-604</sup> 10<sup>-605</sup> 10<sup>-606</sup> 10<sup>-607</sup> 10<sup>-608</sup> 10<sup>-609</sup> 10<sup>-610</sup> 10<sup>-611</sup> 10<sup>-612</sup> 10<sup>-613</sup> 10<sup>-614</sup> 10<sup>-615</sup> 10<sup>-616</sup> 10<sup>-617</sup> 10<sup>-618</sup> 10<sup>-619</sup> 10<sup>-620</sup> 10<sup>-621</sup> 10<sup>-622</sup> 10<sup>-623</sup> 10<sup>-624</sup> 10<sup>-625</sup> 10<sup>-626</sup> 10<sup>-627</sup> 10<sup>-628</sup> 10<sup>-629</sup> 10<sup>-630</sup> 10<sup>-631</sup> 10<sup>-632</sup> 10<sup>-633</sup> 10<sup>-634</sup> 10<sup>-635</sup> 10<sup>-636</sup> 10<sup>-637</sup> 10<sup>-638</sup> 10<sup>-639</sup> 10<sup>-640</sup> 10<sup>-641</sup> 10<sup>-642</sup> 10<sup>-643</sup> 10<sup>-644</sup> 10<sup>-645</sup> 10<sup>-646</sup> 10<sup>-647</sup> 10<sup>-648</sup> 10<sup>-649</sup> 10<sup>-650</sup> 10<sup>-651</sup> 10<sup>-652</sup> 10<sup>-653</sup> 10<sup>-654</sup> 10<sup>-655</sup> 10<sup>-656</sup> 10<sup>-657</sup> 10<sup>-658</sup> 10<sup>-659</sup> 10<sup>-660</sup> 10<sup>-661</sup> 10<sup>-662</sup> 10<sup>-663</sup> 10<sup>-664</sup> 10<sup>-665</sup> 10<sup>-666</sup> 10<sup>-667</sup> 10<sup>-668</sup> 10<sup>-669</sup> 10<sup>-670</sup> 10<sup>-671</sup> 10<sup>-672</sup> 10<sup>-673</sup> 10<sup>-674</sup> 10<sup>-675</sup> 10<sup>-676</sup> 10<sup>-677</sup> 10<sup>-678</sup> 10<sup>-679</sup> 10<sup>-680</sup> 10<sup>-681</sup> 10<sup>-682</sup> 10<sup>-683</sup> 10<sup>-684</sup> 10<sup>-685</sup> 10<sup>-686</sup> 10<sup>-687</sup> 10<sup>-688</sup> 10<sup>-689</sup> 10<sup>-690</sup> 10<sup>-691</sup> 10<sup>-692</sup> 10<sup>-693</sup> 10<sup>-694</sup> 10<sup>-695</sup> 10<sup>-696</sup> 10<sup>-697</sup> 10<sup>-698</sup> 10<sup>-699</sup> 10<sup>-700</sup> 10<sup>-701</sup> 10<sup>-702</sup> 10<sup>-703</sup> 10<sup>-704</sup> 10<sup>-705</sup> 10<sup>-706</sup> 10<sup>-707</sup> 10<sup>-708</sup> 10<sup>-709</sup> 10<sup>-710</sup> 10<sup>-711</sup> 10<sup>-712</sup> 10<sup>-713</sup> 10<sup>-714</sup> 10<sup>-715</sup> 10<sup>-716</sup> 10<sup>-717</sup> 10<sup>-718</sup> 10<sup>-719</sup> 10<sup>-720</sup> 10<sup>-721</sup> 10<sup>-722</sup> 10<sup>-723</sup> 10<sup>-724</sup> 10<sup>-725</sup> 10<sup>-726</sup> 10<sup>-727</sup> 10<sup>-728</sup> 10<sup>-729</sup> 10<sup>-730</sup> 10<sup>-731</sup> 10<sup>-732</sup> 10<sup>-733</sup> 10<sup>-734</sup> 10<sup>-735</sup> 10<sup>-736</sup> 10<sup>-737</sup> 10<sup>-738</sup> 10<sup>-739</sup> 10<sup>-740</sup> 10<sup>-741</sup> 10<sup>-742</sup> 10<sup>-743</sup> 10<sup>-744</sup> 10<sup>-745</sup> 10<sup>-746</sup> 10<sup>-747</sup> 10<sup>-748</sup> 10<sup>-749</sup> 10<sup>-750</sup> 10<sup>-751</sup> 10<sup>-752</sup> 10<sup>-753</sup> 10<sup>-754</sup> 10<sup>-755</sup> 10<sup>-756</sup> 10<sup>-757</sup> 10<sup>-758</sup> 10<sup>-759</sup> 10<sup>-760</sup> 10<sup>-761</sup> 10<sup>-762</sup> 10<sup>-763</sup> 10<sup>-764</sup> 10<sup>-765</sup> 10<sup>-766</sup> 10<sup>-767</sup> 10<sup>-768</sup> 10<sup>-769</sup> 10<sup>-770</sup> 10<sup>-771</sup> 10<sup>-772</sup> 10<sup>-773</sup> 10<sup>-774</sup> 10<sup>-775</sup> 10<sup>-776</sup> 10<sup>-777</sup> 10<sup>-778</sup> 10<sup>-779</sup> 10<sup>-780</sup> 10<sup>-781</sup> 10<sup>-782</sup> 10<sup>-783</sup> 10<sup>-784</sup> 10<sup>-785</sup> 10<sup>-786</sup> 10<sup>-787</sup> 10<sup>-788</sup> 10<sup>-789</sup> 10<sup>-790</sup> 10<sup>-791</sup> 10<sup>-792</sup> 10<sup>-793</sup> 10<sup>-794</sup> 10<sup>-795</sup> 10<sup>-796</sup> 10<sup>-797</sup> 10<sup>-798</sup> 10<sup>-799</sup> 10<sup>-800</sup> 10<sup>-801</sup> 10<sup>-802</sup> 10<sup>-803</sup> 10<sup>-804</sup> 10<sup>-805</sup> 10<sup>-806</sup> 10<sup>-807</sup> 10<sup>-808</sup> 10<sup>-809</sup> 10<sup>-810</sup> 10<sup>-811</sup> 10<sup>-812</sup> 10<sup>-813</sup> 10<sup>-814</sup> 10<sup>-815</sup> 10<sup>-816</sup> 10<sup>-817</sup> 10<sup>-818</sup> 10<sup>-819</sup> 10<sup>-820</</sup>			

PROJECT: 10-1163-0003

## RECORD OF Drillhole: GB-05

SHEET 1 OF 4

LOCATION: N 5033620.4 ;E 434945.7

DRILLING DATE: AUG 18-20, 2011

DATUM:

INCLINATION: -90° AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. (m)	DEPTH (m)	RUN No.	FLUSH RETURN	RECOVERY INDEX PER METER	R.G.D. %	DISCONTINUITY DATA	HYDRAULIC CONDUCTIVITY K.m/sec	WEATH- ERING INDEX	FEATURES	NOTES		
11		Continued from Record of Borehole GB-05		202.62	11.66											
12		11.66 - 26.70 m Moderately weathered, foliated, dark grey to dark reddish brown, fine grained, non-porous, weak to medium strong, RHYOLITE CRYSTAL TUFF (RCTF) -Strong silification, slight sericitic-chlorite alteration, pervasive oxidation -Moderate water loss between 11.89 - 12.22 m (Broken/Lost core zone) -Numerous iron-rich veins between 1 - 40 mm thick		11.66	11.66	1										8c
13	NQ3 BH NO2 Rods Triple Take Sampling															
14																
15																
16																
17																
18		18.48 - 18.55 m Very strongly silified zone containing 3 cm diameter, globular pyrite														8c
19																
20																
21																
CONTINUED NEXT PAGE																

PROJECT: 10-1193-0003

## RECORD OF Drillhole: GB-05

SHEET 2 OF 4

LOCATION: N 5033620.4 ,E 434945.7

DRILLING DATE: AUG 19-20, 2011

DATUM:

INCLINATION: -90° AZIMUTH: --

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. DEPTH (m)	RUN NO.	PLUG RETURNS	RECOVERY TOTAL DORN % SS288	RECOVERY SOLID GORN % SS288	RECOVERY PORE METER GORN % SS288	R.D. %	FRACT. INDEX PEN METER GORN % SS288	DEWALL CORE ANALYSIS GORN % SS288	DISCONTINUITY DATA			HYDRAULIC CONDUCTIVITY K, cm/sec	WEATH- ERING INDEX	FEATURES	NOTES
													PL - Planar	PO - Polished	BR - Broken Rock				
													CU - Curved	K - Smoothed	SM - Smooth				
<b>-- CONTINUED FROM PREVIOUS PAGE --</b>																			
22		11.85 - 26.70 m Moderately weathered, foliated, dark grey to dark reddish brown, fine grained, non-porous, weak to medium strong, RHYOLITE CRYSTAL TUFF (RCTF) -Strong silification, slight sericitic/chlorite alteration, pervasive oxidation -Moderate water loss between 11.89 - 12.22 m (Broken/Lost core zone) -Numerous iron-rich veins between 1 - 40 mm thick	XXX		7									JN, PL, RO, CT, OX, CH JN, PL, SM, DT, OX					
23					8									JN, PL, RO, SA, OX, CH					
24					9									JN, PL, RO, SA, OX, CH					
25		24.99 - 26.70 m Dark green propylitic alteration zone												FO, PL, VR, CT, F, M FO, PL, RO, ST, OX FO, PL, VR, ST, OX					
26														FO, PL, RO, ST, OX					
27		26.70 - 29.70 m Slightly to moderately weathered, massive, greenish black to very dark reddish brown, fine grained, semi-porous, weak to medium strong MAFIC DYKE (MFDK) -Highly chlorite altered, pervasive oxidation -White, randomly oriented veinlets		187.57	26.70									MUR, VR, IN, OX, CL, 1 min FO, PL, VR, CT, OX, CL FO, PL, VR, ST, OX FO, PL, VR, CT, OX, CL FO, PL, VR, CT, OX, CL, 1 min					
28					28									JN, PL, RO, CT, OX, M JN, PL, SM, CT, OX, M JN, PL, NM, CT, OX, M JN, PL, RO, CT, OX, SA					
29					29									SH, PL, K, ST, OX SH, PL, RO, IN, OX, CL, 2 min JN, PL, RO, IN, OX, CL, 2 min JN, PL, SM, CT, OX					
30		29.70 - 41.76 m Slightly weathered, highly foliated, dark grey to dark reddish brown, fine grained, non-porous, weak to medium strong, RHYOLITE CRYSTAL TUFF (RCTF) -Strong to moderate silification, slight sericitic/chlorite alteration, pervasive oxidation -More iron-rich veins to 38.00 m		184.57	30.70									JN, PL, RO, CT, OX, CL JN, PL, RO, IN, OX, CL, 1 min JN, PL, RO, IN, OX, CL, 1 min JN, PL, RO, CT, OX, CH PR, IR, VR, CT, OX					
31					31									JN, PL, RO, CT, OX, M JN, PL, SM, CT, OX, CL					
														SH, PL, K, SA, OX SH, PL, K, SA, OX, CH SH, PL, K, CT, OX SH, PL, K, CT, CH SH, PL, K, CT, CH JN, PL, SM, CT, OX, CH JN, PL, RO, CT, OX, CH					
<b>CONTINUED NEXT PAGE</b>																			

PROJECT: 10-1193-0003

**RECORD OF Drillhole: GB-05**

SHEET 3 OF 4

LOCATION: N 5033620.4 ;E 434945.7

DRILLING DATE: AUG 19-20, 2011

DATUM:

INCLINATION: -90°      AZIMUTH: —

DRILL RIG: D-120

DRILLING CONTR

DRILLING CONTRACTOR: Coleman Engineering Co.

*CONTINUED NEXT PAGE*



DEPTH SCALE

1 : 50

LOGGED: ES

CHECKED:

PROJECT: 10-1193-0003

LOCATION: N 5033620.4 ;E 434945.7

INCLINATION: -80° AZIMUTH: --

## RECORD OF Drillhole: GB-05

SHEET 4 OF 4

DRILLING DATE: AUG 19-20, 2011

DRILL RIG: D-120

DRILLING CONTRACTOR: Coleman Engineering Co.

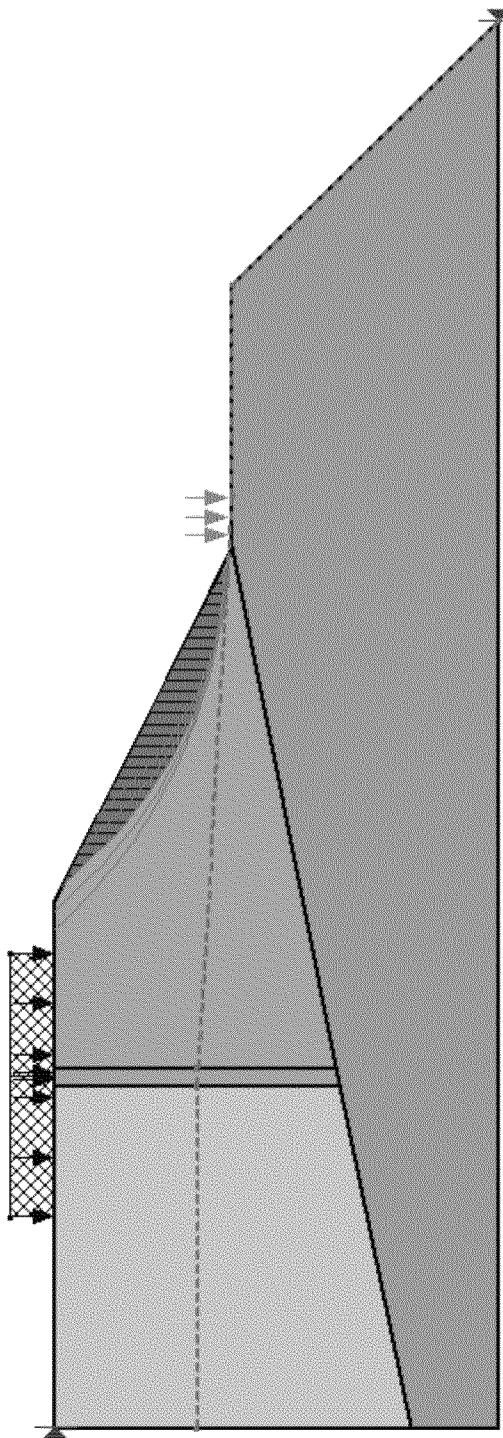
DATUM:

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. (m)	RUN NO.	PUSH RETURN	JN - Joint FLT - Fault SHR - Shear VN - Vein CJ - Coredge	BD - Bedding FO - Faltung CC - Contact OR - Olistosyal CL - Cleavage	PL - Planar CU - Curved UN - Undulating ST - Stepped IR - Irregular	PO - Pointed K - Smooth SM - Smooth Ro - Round MB - Mechanical Break	BR - Broken Rock	NOTES For additional information refer to the of observations & symbols	FEATURES	NOTES	
<b>-- CONTINUED FROM PREVIOUS PAGE --</b>															
42		END OF DRILLHOLE		41.76											
43															
44															
45															
46															
47															
48															
49															
50															
51															
52															
53															
54															
55															
56															
57															
58															
59															
60															
61															

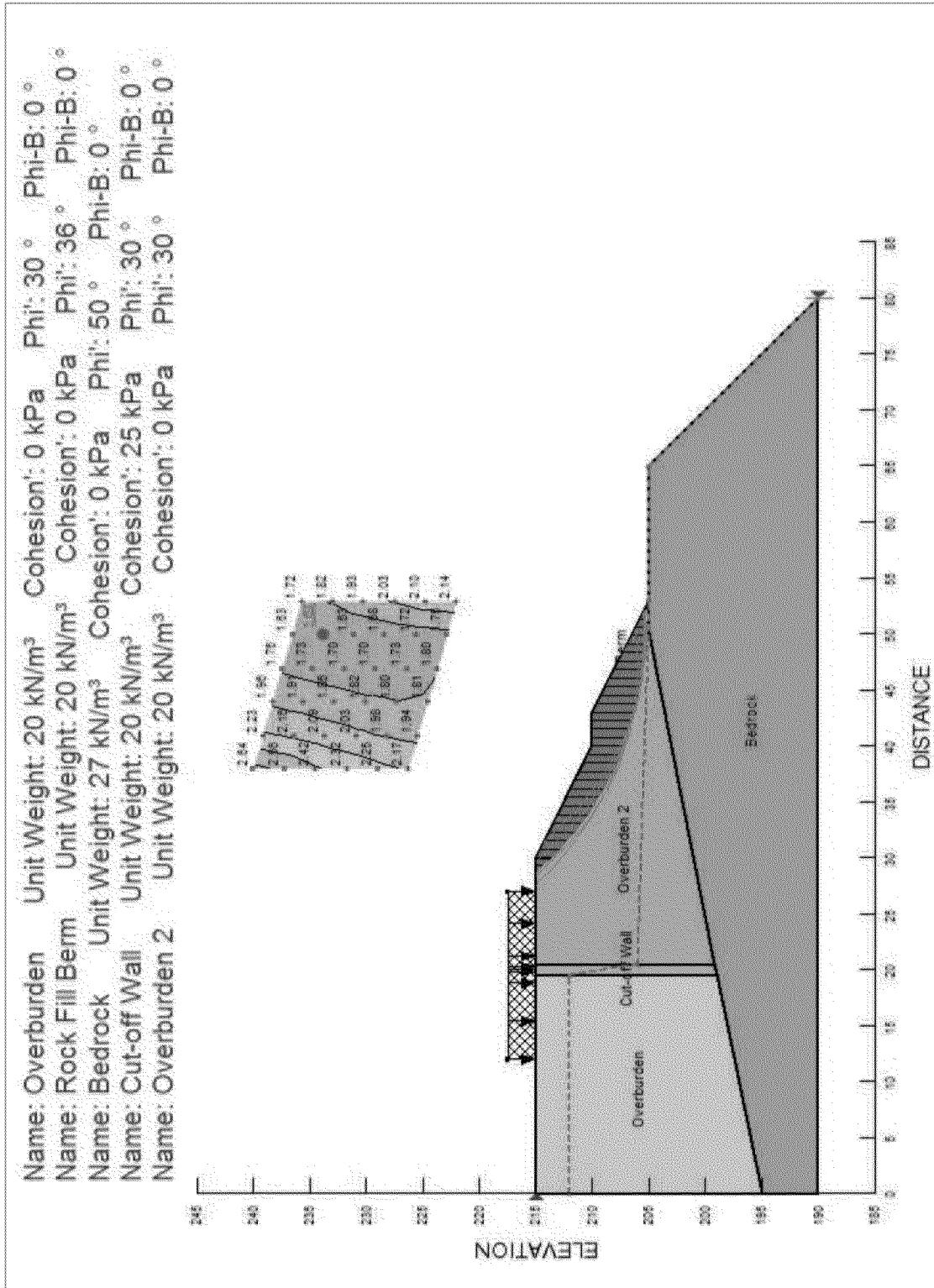
**Attachment 2**  
**Slope Stability Analysis Results**

Name: Overburden      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 30 °      Phi-B: 0 °  
 Name: Bedrock      Unit Weight: 27 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 50 °      Phi-B: 0 °  
 Name: Cut-off Wall      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 30 °      Phi-B: 0 °  
 Name: Overburden 2      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 30 °      Phi-B: 0 °

	2.69	2.15	1.79	1.52	1.34	1.34
*	2.60	2.07	1.71	1.46	1.30	1.34
*	2.51	1.99	1.64	1.41	1.28	1.42
*	2.41	1.91	1.64	1.41	1.28	1.53
*	2.32	1.83	1.58	1.37	1.27	1.27
*	2.23	1.75	1.51	1.34	1.28	1.70
*	2.15	1.75	1.47	1.33	1.28	1.96
*	2.07	1.75	1.47	1.33	1.28	2.36

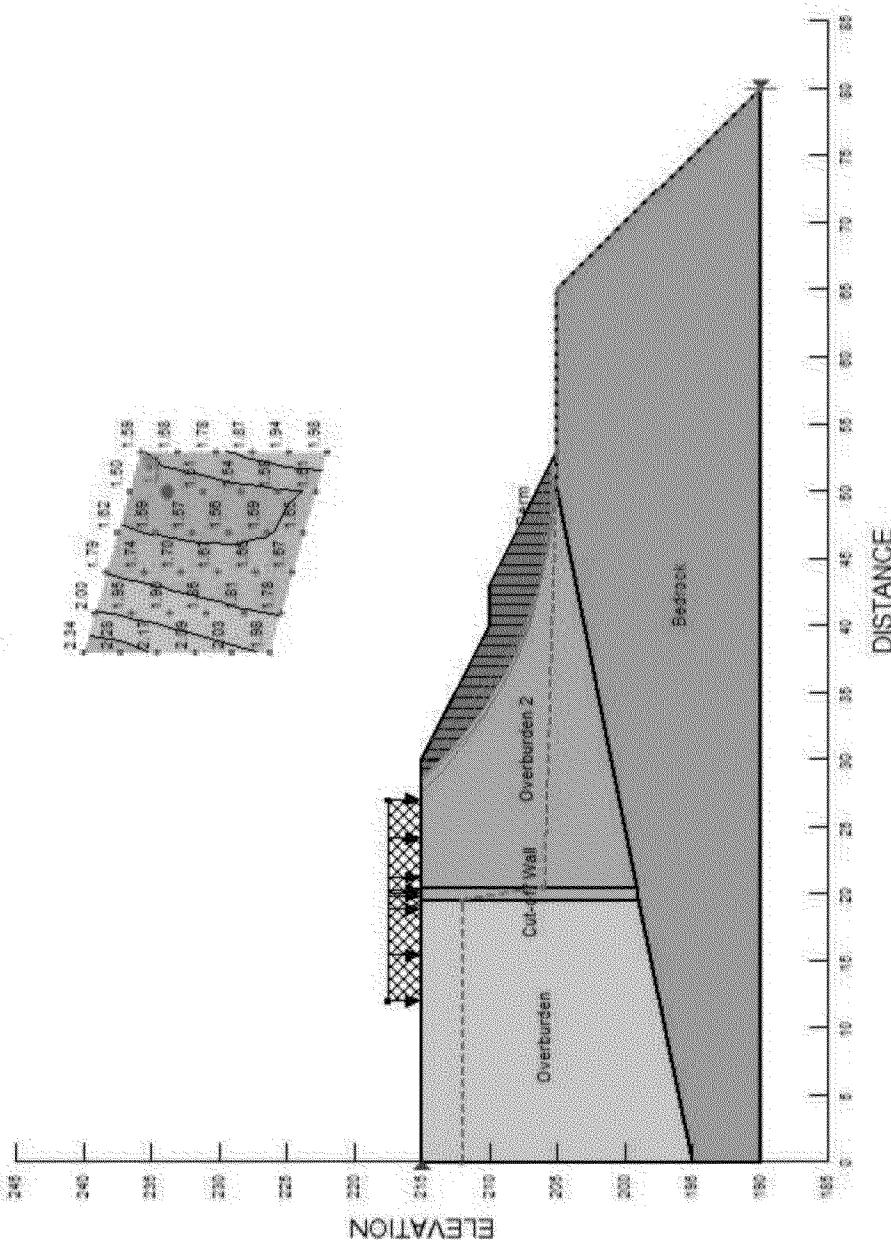
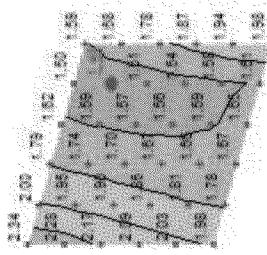


Slope Stability Analysis Result - Static Short Term Condition during Construction



Slope Stability Analysis Result - Static Steady State with a 100-year, 24-hour storm event

Name: Overburden      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 30 °      Phi-B: 0 °  
 Name: Rock Fill Berm      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 36 °      Phi-B: 0 °  
 Name: Bedrock      Unit Weight: 27 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 50 °      Phi-B: 0 °  
 Name: Cut-off Wall      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 25 kPa      Phi: 30 °      Phi-B: 0 °  
 Name: Overburden 2      Unit Weight: 20 kN/m<sup>3</sup>      Cohesion: 0 kPa      Phi: 30 °      Phi-B: 0 °



Slope Stability Analysis Result - Pseudo-Static Long Term Condition with PGA = 0.03 g.